

CrossMark
click for updates

Cite this article: Cohen Y, Rothman DH. 2015 Mechanisms for mechanical trapping of geologically sequestered carbon dioxide. *Proc. R. Soc. A* **471**: 20140853.
<http://dx.doi.org/10.1098/rspa.2014.0853>

Received: 3 November 2014

Accepted: 19 December 2014

Subject Areas:

geophysics, fluid mechanics, geochemistry

Keywords:

reactive transport model, carbon sequestration, Grotthuss mechanism, structural diffusion, invasion percolation, self-sealing

Author for correspondence:

Yossi Cohen

e-mail: ycohen@mit.edu

Electronic supplementary material is available at <http://dx.doi.org/10.1098/rspa.2014.0853> or via <http://rspa.royalsocietypublishing.org>.

Mechanisms for mechanical trapping of geologically sequestered carbon dioxide

Yossi Cohen and Daniel H. Rothman

Lorenz Center, Department of Earth Atmospheric and Planetary Sciences, Massachusetts Institute of Technology, Cambridge, MA 02139, USA

Carbon dioxide (CO₂) sequestration in subsurface reservoirs is important for limiting atmospheric CO₂ concentrations. However, a complete physical picture able to predict the structure developing within the porous medium is lacking. We investigate theoretically reactive transport in the long-time evolution of carbon in the brine–rock environment. As CO₂ is injected into a brine–rock environment, a carbonate-rich region is created amid brine. Within the carbonate-rich region minerals dissolve and migrate from regions of high-to-low concentration, along with other dissolved carbonate species. This causes mineral precipitation at the interface between the two regions. We argue that precipitation in a small layer reduces diffusivity, and eventually causes mechanical trapping of the CO₂. Consequently, only a small fraction of the CO₂ is converted to solid mineral; the remainder either dissolves in water or is trapped in its original form. We also study the case of a pure CO₂ bubble surrounded by brine and suggest a mechanism that may lead to a carbonate-encrusted bubble owing to structural diffusion.

1. Introduction

The sequestration of CO₂ in geological formations is widely considered to be an important approach for mitigating the rise of atmospheric CO₂ levels [1–5]. Deep saline aquifers and gas fields are primarily chosen for storage [1,4,6]. Supercritical CO₂ is injected into these porous media while displacing another fluid, brine [5,7]. The propagation of the CO₂ through the reservoir displays a variety of fluid-dynamical instabilities [8,9]. After injection and the cessation of buoyancy-driven flow, chemical dissolution and precipitation dominate

© 2015 The Authors. Published by the Royal Society under the terms of the Creative Commons Attribution License <http://creativecommons.org/licenses/by/4.0/>, which permits unrestricted use, provided the original author and source are credited.

the ensuing evolution of the reservoir. This late stage of the evolution, which remains poorly understood [10,11], is the focus of this paper.

As the CO₂ is injected into the brine–rock environment, it initially becomes trapped, either by a physical mechanism in the presence of low permeability rocks, or by retention as a separate phase in the pore space owing to interfacial tension [12]. The disordered structure of the void spaces forces the injected fluid along certain paths that create regions, or bubbles, of the injected fluid amid regions of the defending fluid, and vice versa [13–16]. This process is known as invasion percolation when, as for the supercritical CO₂, the invading fluid is non-wetting. For two immiscible fluids, the fluid configuration is often determined by the structure of the rock and by surface tension effects [8]. Further, the two-phase system can become unstable when reactant particles migrate from one phase to the other and change the chemical composition of each phase [10,17]. Within the high CO₂ phase, minerals dissolve [18,19]; diffusion causes minerals and carbonate species to migrate from high-to-low concentration regions, and a fraction of them precipitates [18]. In nature, this process can be seen in hot springs, when a bubble of oxygen emerges from photosynthetic cyanobacteria [20,21]. The high gradient of CO₂ between the bubble and the surrounding water leads to loss of CO₂ in the vicinity of the bubble, drives up the saturation level and eventually a crust is created around the bubble. In general, mineral precipitation on a small boundary layer at the interface may lead to lower diffusivity and slower kinetics. In the carbon sequestration process, this may cause a mechanical trapping of the CO₂ bubble and lower the solidification rate of the carbon minerals.

Here, we develop theoretical understanding of this process of mechanical phase separation. We consider two scales: at the microscale, a single CO₂ bubble is surrounded by brine in the void space of a porous medium. In this case, the reactions occur at the interface between the bubble and the brine, as the CO₂ dissolves and reduces the pH in its vicinity. The macroscale averages over many such bubbles. In this case, a high concentration of the invaded CO₂ changes the properties of a macroscopic region. The region becomes more acidic, and no precipitation occurs unless the carbonate species migrate to a different region.

This paper begins by addressing the macroscale problem and the mathematical background of the reactive diffusion equation. We then study the mobility change in the fluid–rock system owing to the precipitate minerals. Finally, we consider the microscale case of a single CO₂ bubble amid brine and suggest a second mechanism that may also lead to separation and self-sealing.

2. Macroscopic reactive transport

The injection of supercritical CO₂ (scCO₂) into a porous medium, initially occupied with another fluid, i.e. brine (salty water), generates two different regions in the system [11,17,22]. The first region is where the CO₂ displaced most of the existing brine. In this region, the void space in the porous medium is filled with bubbles of CO₂ and water saturated with carbonate species. The CO₂ dissolves rapidly in the water to reach equilibrium which results in low pH, and also a high concentration of dissolved minerals [23,24]. The second region is the intact brine–rock system, which is characterized by a low concentration of CO₂ and higher pH. Figure 1 depicts the complexity of the CO₂–brine–rock system.

The existence of two phases and concentration gradients drives the components to migrate from one phase to another. As they diffuse, they react to reach a local equilibrium. Although pure scCO₂ may be clogged owing to mechanical or capillary trapping [1,26], in the presence of water, it can dissolve into its ionic forms, i.e. bicarbonate and carbonic acid, until it reaches a local thermodynamical equilibrium [27]. These carbonate species may diffuse more easily through the brine. Within the high CO₂ phase, minerals dissolve because of the acidic environment. They then migrate from high-to-low concentration regions and a fraction of them precipitates. The evolution of each component can be described by the reactive diffusion equation

$$\frac{\partial C_i}{\partial t} = \nabla \cdot (D_i \nabla C_i) + R_i(C_1, C_2, \dots, C_5). \quad (2.1)$$

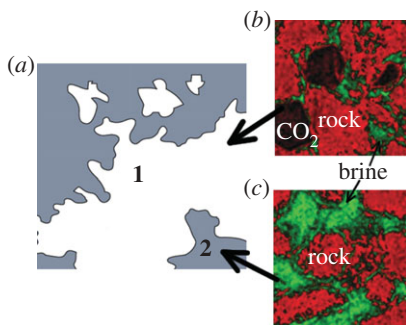


Figure 1. *Macroscale:* (a) Irregularly shaped regions of brine (grey) amid carbonate-rich regions (white) [17]. *Microscale:* CT image of material distribution in Frio sandstone, adapted from reference [25]. (b) Region 1 consists of CO₂ bubbles surrounded by brine and grains of the rock. (c) Region 2 is the brine–rock system. (Online version in colour.)

Here, the C_i , $i = 1, \dots, 5$ are the concentration of the CO₂, HCO₃⁻, CO₃²⁻, H⁺ and the mineral Ca²⁺, respectively. D_i is the isotropic diffusion coefficient for the i th component, and R_i is the reaction rate defined by the carbonate system [27,28] and the dissolution and precipitation of calcite mineral. The latter can be expressed as [29–31]

$$\frac{dM}{dt} = -k_m(1 - \Omega), \quad (2.2)$$

where M represents the density of precipitated calcite. The rate coefficient is defined by [30]

$$k_m = A(\mathbf{r}, t)(k_{+1}[\text{H}^+] + k_{+2}[\text{CO}_2] + k_{+3}), \quad (2.3)$$

where $A(\mathbf{r}, t)$ is the reactive surface area, and k_{+i} are the rate constants for the forward reactions. The saturation ratio [29]

$$\Omega = \frac{[\text{Ca}^{2+}][\text{CO}_3^{2-}]}{K_{sp}} \quad (2.4)$$

is defined by the ion activity product divided by the solubility constant of calcite. Details of the reactions and the values of the reaction constants can be found in the electronic supplementary material. Whether the calcite will precipitate or dissolve is determined by the value of Ω ; when $\Omega < 1$, dissolution occurs; when $\Omega > 1$, mineral precipitates and when $\Omega = 1$, the system is at equilibrium.

3. Numerical simulation

In our model, we assume that there is no diffusion of the solid mineral as it nucleates and precipitates at the surface of the rock. In addition, the capillary forces between the scCO₂ and the water prevent the mixing between the two phases; therefore, the diffusion constant of CO₂ is also set to zero. Because the dissolution of calcite is considerably fast compared with dissolution of other minerals, we assume that, after injection, calcite dissolves quickly until it reaches equilibrium. Only new calcite that has been precipitated can be dissolved again. Thus, the reactive surface area is set to zero, as long as there is no previous precipitation of calcite. In other words, we set $A(\mathbf{r}, t) = 0$, when $M(\mathbf{r}, t) = 0$ and $\Omega(\mathbf{r}, t) < 1$, and $A(\mathbf{r}, t) = 1$ otherwise.

We solve the reactive diffusion equations (2.1) and (2.2) for each component using the Galerkin finite-elements method on quadratic triangular grid with a fourth-order Runge–Kutta integration scheme. The simulation starts when the carbonate system, the pH and the dissolved calcium mineral are at local equilibrium in each phase. In region 1, the carbonate-rich brine–rock region (figure 1), we set the pH to 6 and the total dissolved inorganic carbon to $10^{-2} \text{ mol l}^{-1}$. In region 2, we set pH = 7 and the carbonate concentration at $10^{-3} \text{ mol l}^{-1}$. We apply reflective boundary conditions far from the interface between the two regions. During the simulation,

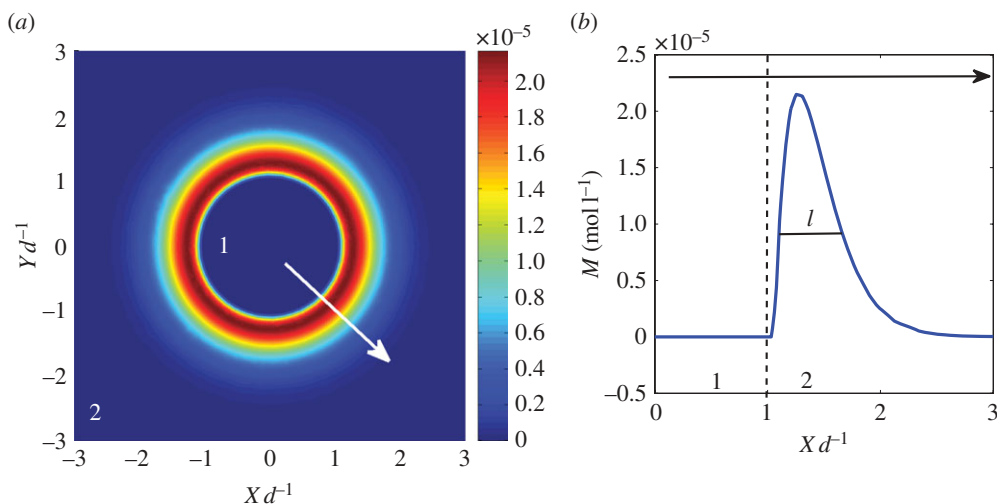


Figure 2. (a) Mineral precipitation on the periphery of a circular domain ($d = 2$ cm). In the inner shape is the carbonate-rich phase (region 1) which consists of high concentration of CO_2 , amid region 2, the brine. Precipitation of minerals occurs at the interface that separates the two regions. The colour indicates the accumulation of precipitated minerals. The lengths are normalized by d , a characteristic length of region 1, and given in dimensionless units. (b) The profile of the accumulated mineral at $t = 0.5 d^2/D$. The dashed line separates the two regions and the black arrow corresponds to the white arrow in (a). (Online version in colour.)

the concentrations at the boundary remain effectively constant. The simulation starts with the concentration of each one of the carbonate species and the dissolved calcium mineral at local equilibrium in each region.

We consider a carbonate-rich circular shape (region 1) surrounded by brine (region 2). We find that the accumulation of calcite, shown in figure 2a, occurs on a small boundary layer close to the interface. The precipitation profile is approximated by the typical diffusion length, $l \sim \sqrt{Dt}$, shown in figure 2b. However, when the contribution of the reaction terms becomes significant, we see deviations from this profile. To approximate the time scale over which this profile holds, we consider the reactive diffusion equation, equation (2.1), and the accumulation of precipitated mineral in equation (2.2). Changing equation (2.1) into dimensionless variables, $x \rightarrow \xi d$, $t \rightarrow (d^2/D)\tau$, leads to

$$\frac{\partial C_i}{\partial \tau} = \frac{\partial^2 C_i}{\partial \xi^2} + \frac{d^2}{D} R_i(C_j), \quad j = 1, \dots, 5. \quad (3.1)$$

where d is the effective domain size of region 1 that participates in the dynamics. From equation (2.2), the density of the precipitated mineral becomes

$$\frac{dM}{d\tau} = -\frac{k_m d^2}{D} \left(1 - \frac{A(\tau)B(\tau)}{K_{sp}} \right), \quad (3.2)$$

where $A(\tau)$ and $B(\tau)$ correspond to the concentration of Ca^{2+} and CO_3^{2-} . As long as $A(\tau)$ and $B(\tau)$ are purely diffusion-controlled, the system is self-similar, and the precipitation profile (figure 2b) holds. When the reaction term becomes dominant, a deviation from this profile will be obtained. From the numerics, the concentration of CO_3^{2-} is likely to deviate first from this behaviour after $\tau \sim d^2/D$ owing to its low concentration in the brine. The kinetics are described in detail in the electronic supplementary material.

Figure 3 shows qualitatively how the interface curvature alters the mineral precipitation. We find that the accumulated crust is highly dependent on the curvature of the interface owing to the nature of a diffusion process through a curved interface [32]. Initially, accumulation of mineral is

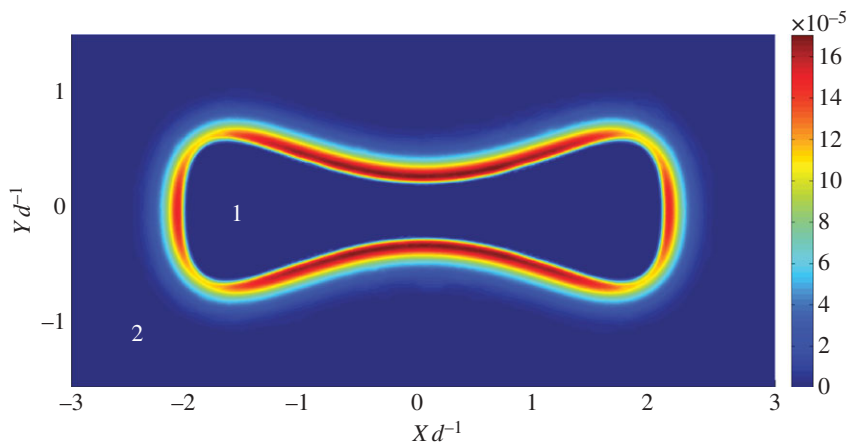


Figure 3. The same as figure 2a, but with an interface of variable curvature. Precipitation is greatest in regions of high negative curvature (concave outwards). (Online version in colour.)

effectively diffusion-controlled. Thus, negative curvature with respect to the inner bubble of the CO_2 phase has maximum mineral precipitation at the interface, owing to the convergence of lines of flux [32,33].

Collectively, these results indicate that precipitation of mineral occurs on a small boundary layer at the interface and a carbonate crust, created in a small boundary layer, can lead to a mechanical separation of the two phases.

4. System size dependence

Mineral precipitation along the interface changes the porosity of the rock, decreases the effective diffusivity, and may clog existing voids [1,26]. The decrease in the mobility of the ions in the solution could bring further solidification of minerals to a halt. Whether a pathway between pores will be clogged or not is highly dependent on the local density of the accumulated mineral, which depends also on the amount of the carbonate species, and the size and the shape of the domain noted as region 1. To study how a change in the size alters the maximum mineral density, we initiate a one-dimensional domain of size d of region 1, and run the simulation until equilibrium. During the simulation, the mineral density reaches a maximum and then decreases as the solution at the interface become more acidic, shown in figure 4. We calculate the maximum calcite concentration M as a function of d . We obtain a power law relationship $M \propto d^n$, where $n \simeq 1.72$, as shown in figure 5.

The exponent n can be approximated by a simple scaling analysis. If $A(\tau)$ and $B(\tau)$ in equation (3.2) are purely diffusion-controlled, i.e. if the reaction term in equation (3.1) can be neglected, the accumulated precipitation scales like d^2 . In practice, the exponent may be lower than 2 because of the contribution of the reaction terms that change the equilibrium state in our system.

5. Effective diffusivity

The diffusivity in a porous medium depends on several factors which are related to the pore geometry and the effective porosity accessible by diffusion [34,35]. For the sake of simplicity, we consider the permeability reduction to be linear with the porosity loss and mineral precipitation, and the effective diffusivity D_e to be linear with the porosity ϕ_t :

$$D_e \propto \phi_t D_0, \quad \phi_t = \left(1 - \frac{\theta}{\theta_c}\right), \quad (5.1)$$

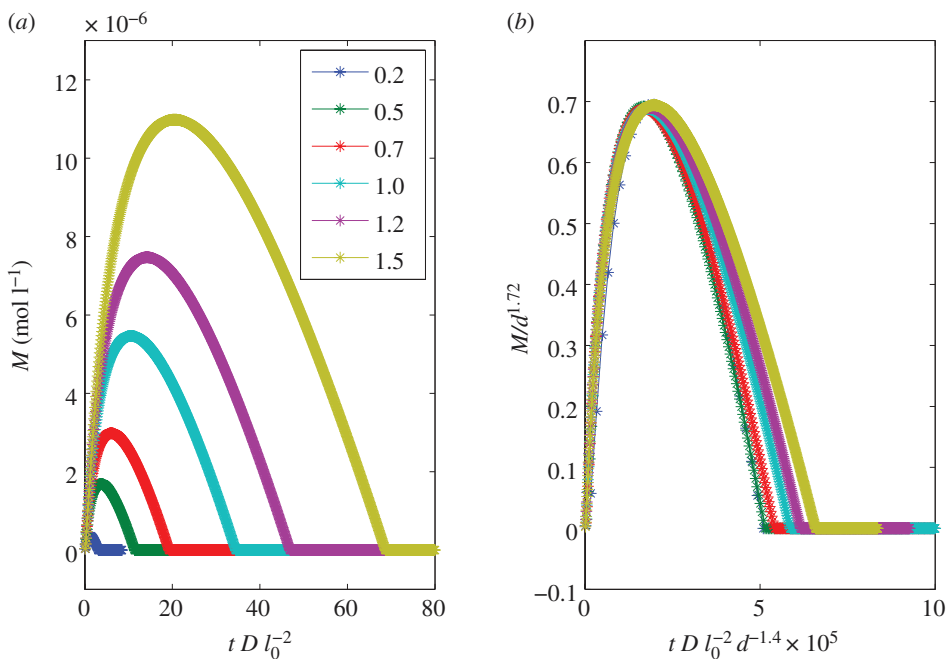


Figure 4. (a) Temporal dependence of the precipitated mineral at the interface for different system size, d , given in the legend in millimetres. The length $l_0 = 1$ mm. (b) Collapse of the data shown on the left side by rescaling the mineral density and time. The exponents are chosen such the maximum mineral density for different bubble sizes occurs at the same position in the rescaled coordinates. (Online version in colour.)

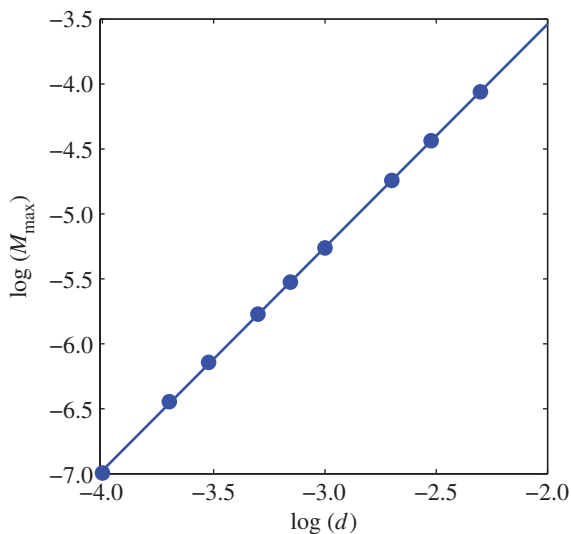


Figure 5. Maximum density of precipitated mineral with respect to system size. The slope is $n = 1.72$. (Online version in colour.)

where D_0 is the bulk diffusivity corresponding to the initial porosity, ϕ_t is the porosity available for transport, $\theta = M$ is the maximum density of the precipitated mineral and θ_c is a critical accumulated density in which D_e vanishes.

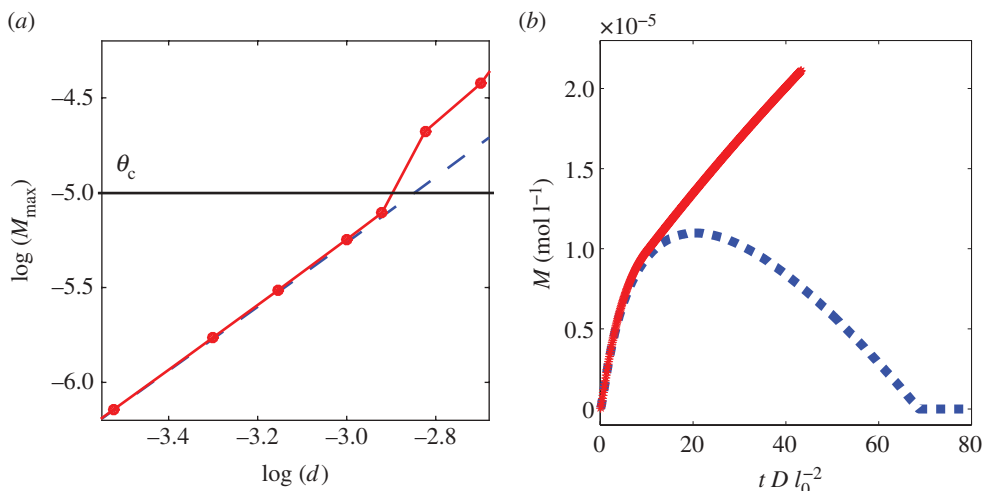


Figure 6. (a) Maximum density of precipitated mineral M with respect to system size d , with clogging. *Dashed line:* the same as figure 5 with $D_e = D_0$. *Solid line:* the results allowing the porosity to decrease and the effective diffusivity D_e to decrease as the precipitation grows. Note the enhanced precipitation when the critical accumulated density, θ_c , is reached. At this point, particles cannot cross between the regions, and the system seeks a local chemical equilibrium. (b) Temporal dependence of precipitated minerals. *Dashed line:* the same as in figure 4. *Solid line:* with clogging. Note that after the diffusivity is reduced to zero, around $t \sim 12$, the two regions are separated and the system seeks local chemical equilibrium. Then, the dynamics stop. (Online version in colour.)

As the accumulated mineral reaches the critical porosity, it changes locally the permeability and mechanical separation may occur owing to diffusivity loss and self-sealing. We also observe that while the diffusion coefficient decreases, it creates even more precipitation in a smaller area close to the interface. These results, shown in figure 6, are in agreement with the diffusion length scale of $l \sim \sqrt{D_e t}$ from the numerical approximation and the mineral precipitation of $M \sim 1/D_e$ from equation (3.2). In addition, when the system is clogged, i.e. when the effective diffusivity goes to zero, the system seeks a local chemical equilibrium.

From the numerical results, we can identify two trapping mechanisms that occur as particles migrate from one region to the other. For small carbonate-rich regions, the CO_2 dissolves completely into the brine, and the low pH does not allow a significant precipitation of the carbonate minerals. Thus, the CO_2 is trapped in its dissolved forms. For larger regions, solidification of minerals stops as clogging occurs, and the developed crust separates the two regions. In both cases, the total amount of the precipitated carbonate minerals is small compared with concentrations of the other carbonate species.

6. The microscale: a single carbon dioxide bubble

Here, we discuss a mechanism that leads to a carbonate-encrusted bubble in which a single bubble of pure CO_2 surrounded by brine develops a crust at the interface. Unlike the upscaled case discussed above, where each region consists of the same ingredients but with a different concentration, here we have a pure bubble (no upscaling) with only CO_2 , either in a liquid phase or gas phase. The problem is pictured in figure 7. In this case, no chemical reactions occur inside the CO_2 bubble; reactions instead occur only at the interface with the brine. The CO_2 then dissolves into the brine, creates charged carbonate species and reduces the pH in its vicinity. Most of the components diffuse slowly away from the interface; however, the protons in water diffuse faster owing to structural diffusion, also known as the Grotthuss mechanism [36]. The concentration gradient with unequal diffusivities generates an electrical field that slows down the

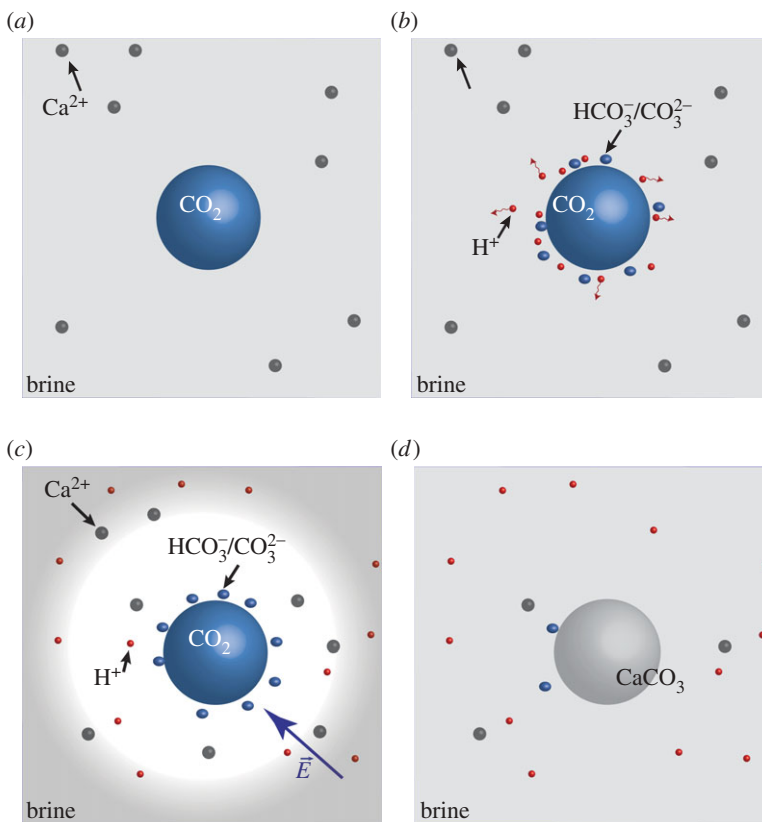


Figure 7. Evolution of a CO₂ bubble (not in scale): (a) a single bubble of pure CO₂ surrounded by brine. (b) At the interface, the CO₂ dissolves into the brine, and reduces the pH. (c) Protons migrate faster from the interface, creating an electrostatic dipole and attracting minerals towards the interface. (d) Minerals precipitate owing to supersaturation, and a crust is created. (Online version in colour.)

rapidly diffusing protons, but also attracts positively charged minerals towards the interface. (The dynamics is described by the Nernst–Planck equations [37,38]). This leads to supersaturation at the interface and mineral precipitation. This process suggests that an isolated bubble can remain stable owing to a self-sealing mechanism. The actual determination whether a bubble will be encrusted or not depends on the environment and the dynamical behaviour of the bubble. First, the velocity of the bubble should be effectively zero or smaller than the mobility of the ions in the solution in order to build the electrostatic field in the vicinity of the bubble. Second, the amount of mineral cations that are attracted to the interface owing to the electrostatic field should suffice to reach supersaturation that causes precipitation. Third, to seal a bubble, the field must be homogeneous in order to create a uniform and stable crust. A quantitative measure of the conditions that lead to self-sealing could be obtained by experiment.

7. Discussion and conclusion

We have shown that in a system of reactive fluids, a gradient in the concentration between regions leads to a supersaturation at the interface and to precipitation and porosity loss. A local change in the porosity reduces permeability and may cause mechanical separation. This process is important in understanding the long-term sequestration of carbon dioxide in subsurface geological formation. We predict that a small domain of a region consisting mostly of the carbonate species in an acidic environment will dissolve completely into the brine. Larger

domains are more likely to be self-sealed, and only a fraction of the carbonate species will be precipitated. For a single CO₂ bubble in brine solution, we suggest a mechanism that causes self-sealing owing to the pH gradient at the interface of the bubble and structural diffusion.

Our results suggest that only a small fraction of the injected CO₂ is converted to a solid mineral. The remainder stays in its dissolved ionic form or is trapped in its original form. Whether a domain will go into dissolution trapping or mechanical separation depends on the concentration gradients, the properties of the rock and the porosity available for transport.

Data accessibility. The data supporting this article have been uploaded as part of the electronic supplementary material.

Acknowledgements. We thank M. Z. Bazant, A. Kudrolli and S. R. Pride for sharing their thoughts and helpful discussions.

Authors' contributions. Y.C. and D.H.R. contributed equally to this work.

Funding statement. The work was supported by the Center for Nanoscale Control of Geologic CO₂, an Energy Frontier Research Center funded by the US Department of Energy, Office of Science, Office of Basic Energy Sciences under Award no. DE-AC02-05CH11231, subcontract 6896518.

Conflict of interests. The authors declare no conflicts of interest.

References

- Metz B, Davidson O, De Coninck HC, Loos M, Meyer LA. 2005 *IPCC special report on carbon dioxide capture and storage: prepared by Working Group III of the Intergovernmental Panel on Climate Change*. Cambridge, UK: IPCC, Cambridge University Press, 4.
- Schrag DP. 2007 Preparing to capture carbon. *Science* **315**, 812–813. (doi:10.1126/science.1137632)
- Bachu S, Gunter WD, Perkins EH. 1994 Aquifer disposal of CO₂: hydrodynamic and mineral trapping. *Energy Convers. Manage.* **35**, 269–279. (doi:10.1016/0196-8904(94)90060-4)
- Lackner KS. 2003 A guide to CO₂ sequestration. *Science* **300**, 1677–1678. (doi:10.1126/science.1079033)
- Song J, Zhang D. 2013 Comprehensive review of caprock-sealing mechanisms for geologic carbon sequestration. *Environ. Sci. Technol.* **47**, 9–22. (doi:10.1021/es301610p)
- Bachu S, Adams JJ. 2003 Sequestration of CO₂ in geological media in response to climate change: capacity of deep saline aquifers to sequester CO₂ in solution. *Energy Convers. Manage.* **44**, 3151–3175. (doi:10.1016/S0196-8904(03)00101-8)
- Chiquet P, Broseta D, Thibeau S. 2007 Wettability alteration of caprock minerals by carbon dioxide. *Geofluids* **7**, 112–122. (doi:10.1111/j.1468-8123.2007.00168.x)
- Huppert HE, Neufeld JA. 2014 The fluid mechanics of carbon dioxide sequestration. *Annu. Rev. Fluid Mech.* **46**, 255–272. (doi:10.1146/annurev-fluid-011212-140627)
- MacMinn CW, Juanes R. 2013 Buoyant currents arrested by convective dissolution. *Geophys. Res. Lett.* **40**, 2017–2022. (doi:10.1002/grl.50473)
- Noiriel C, Steefel CI, Yang L, Ajo-Franklin J. 2012 Upscaling calcium carbonate precipitation rates from pore to continuum scale. *Chem. Geol.* **318**, 60–74. (doi:10.1016/j.chemgeo.2012.05.014)
- Kampman N, Bickle M, Wigley M, Dubacq B. 2014 Fluid flow and CO₂-fluid-mineral interactions during CO₂-storage in sedimentary basins. *Chem. Geol.* **369**, 22–50. (doi:10.1016/j.chemgeo.2013.11.012)
- Gunter WD, Bachu S, Benson S. 2004 The role of hydrogeological and geochemical trapping in sedimentary basins for secure geological storage of carbon dioxide. *Geol. Soc. Lond. (Special Publications)* **233**, 129–145. (doi:10.1144/GSL.SP.2004.233.01.09)
- Dias MM, Wilkinson D. 1986 Percolation with trapping. *J. Physics A, Math. Gen.* **19**, 3131. (doi:10.1088/0305-4470/19/15/034)
- Stauffer D, Aharony A. 1992 *Introduction to percolation theory*. London, UK: Taylor and Francis.
- Wilkinson D, Willemsen JF. 1983 Invasion percolation: a new form of percolation theory. *J. Physics A, Math. Gen.* **16**, 3365. (doi:10.1088/0305-4470/16/14/028)
- Feder J. 1988 *Fractals, 1988*. New York, NY: Plenum Press.
- Reeves D, Rothman DH. 2012 Impact of structured heterogeneities on reactive two-phase porous flow. *Phys. Rev. E* **86**, 031120. (doi:10.1103/PhysRevE.86.031120)

18. Kelemen PB, Matter J, Streit EE, Rudge JF, Curry WB, Blusztajn J. 2011 Rates and mechanisms of mineral carbonation in peridotite: natural processes and recipes for enhanced, in situ CO₂ capture and storage. *Annu. Rev. Earth Planet. Sci.* **39**, 545–576. (doi:10.1146/annurev-earth-092010-152509)
19. Rudge JF, Kelemen PB, Spiegelman M. 2010 A simple model of reaction-induced cracking applied to serpentinization and carbonation of peridotite. *Earth Planet. Sci. Lett.* **291**, 215–227. (doi:10.1016/j.epsl.2010.01.016)
20. Chafetz H, Rush PF, Utech NM. 1991 Microenvironmental controls on mineralogy and habit of CaCO₃ precipitates: an example from an active travertine system. *Sedimentology* **38**, 107–126. (doi:10.1111/j.1365-3091.1991.tb01857.x)
21. Fouke BW, Farmer JD, Des Marais DJ, Pratt L, Sturchio NC, Burns PC, Discipulo MK. 2000 Depositional facies and aqueous-solid geochemistry of travertine-depositing hot springs (Angel Terrace, Mammoth hot Springs, Yellowstone National Park, U.S.A.). *J. Sediment. Res.* **70**, 565–585. (doi:10.1306/2DC40929-0E47-11D7-8643000102C1865D)
22. Tsai PA, Riesing K, Stone HA. 2013 Density-driven convection enhanced by an inclined boundary: implications for geological CO₂ storage. *Phys. Rev. E* **87**, 011003. (doi:10.1103/PhysRevE.87.011003)
23. Liu Q, Mercedes Maroto-Valer M. 2010 Investigation of the pH effect of a typical host rock and buffer solution on CO₂ sequestration in synthetic brines. *Fuel Process. Technol.* **91**, 1321–1329. (doi:10.1016/j.fuproc.2010.05.002)
24. Kharaka YK, Cole DR, Hovorka SD, Gunter WD, Knauss KG, Freifeld BM. 2006 Gas–water–rock interactions in frio formation following CO₂ injection: implications for the storage of greenhouse gases in sedimentary basins. *Geology* **34**, 577–580. (doi:10.1130/G22357.1)
25. Silin D, Tomutsa L, Benson SM, Patzek TW. 2011 Microtomography and pore-scale modeling of two-phase fluid distribution. *Trans. Porous Media* **86**, 495–515. (doi:10.1007/s11242-010-9636-2)
26. Matter JM, Kelemen PB. 2009 Permanent storage of carbon dioxide in geological reservoirs by mineral carbonation. *Nat. Geosci.* **2**, 837–841. (doi:10.1038/ngeo683)
27. Zeebe RE, Wolf-Gladrow DA. 2001 *CO₂ in seawater: equilibrium, kinetics, isotopes: equilibrium, kinetics, isotopes*. Amsterdam, The Netherlands: Elsevier.
28. Druckenmiller ML, Mercedes Maroto-Valer M. 2005 Carbon sequestration using brine of adjusted pH to form mineral carbonates. *Fuel Process. Technol.* **86**, 1599–1614. (doi:10.1016/j.fuproc.2005.01.007)
29. Plummer LN, Wigley TML, Parkhurst DL. 1978 The kinetics of calcite dissolution in CO₂-water systems at 5 degrees to 60 degrees C and 0.0 to 1.0 atm CO₂. *Am. J. Sci.* **278**, 179–216. (doi:10.2475/ajs.278.2.179)
30. Chou LEI, Garrels RM, Wollast R. 1989 Comparative study of the kinetics and mechanisms of dissolution of carbonate minerals. *Chem. Geol.* **78**, 269–282. (doi:10.1016/0009-2541(89)90063-6)
31. DePaolo DJ. 2011 Surface kinetic model for isotopic and trace element fractionation during precipitation of calcite from aqueous solutions. *Geochim. Cosmochim. Acta* **75**, 1039–1056. (doi:10.1016/j.gca.2010.11.020)
32. Blyth MG, Pozrikidis C. 2003 Heat conduction across irregular and fractal-like surfaces. *Int. J. Heat Mass Transfer* **46**, 1329–1339. (doi:10.1016/S0017-9310(02)00419-2)
33. Brown HT, Escombe F. 1900 Static diffusion of gases and liquids in relation to the assimilation of carbon and translocation in plants. *Proc. R. Soc. Lond. A* **67**, 124–128. (doi:10.1098/rspl.1900.0009)
34. Sahimi M. 2012 *Flow and transport in porous media and fractured rock: from classical methods to modern approaches*. Weinheim, Germany: John Wiley & Sons.
35. Sahimi M, Jue VL. 1989 Diffusion of large molecules in porous media. *Phys. Rev. Lett.* **62**, 629. (doi:10.1103/PhysRevLett.62.629)
36. Agmon N. 1995 The Grotthuss mechanism. *Chem. Phys. Lett.* **244**, 456–462. (doi:10.1016/0009-2614(95)00905-J)
37. Ramírez P, Alcaraz A, Mafé S. 1997 Effects of pH on ion transport in weak amphoteric membranes. *J. Electroanal. Chem.* **436**, 119–125. (doi:10.1016/S0022-0728(97)00310-0)
38. Andersen MB, Van Soestbergen M, Mani A, Bruus H, Biesheuvel PM, Bazant MZ. 2012 Current-induced membrane discharge. *Phys. Rev. Lett.* **109**, 108301. (doi:10.1103/PhysRevLett.109.108301)